

Geologic carbon storage is unlikely to trigger large earthquakes and reactivate faults through which CO₂ could leak

Victor Vilarrasa^{a,b,1} and Jesus Carrera^c

^aEarth Sciences Division, Lawrence Berkeley National Laboratory, Berkeley, CA 94720; ^bSoil Mechanics Laboratory, Ecole Polytechnique Fédérale de Lausanne, 1015 Lausanne, Switzerland; and ^cGrup d'Hidrologia Subterrània (GHS), Institute of Environmental Assessment and Water Research, Consejo Superior de Investigaciones Científicas, 08034 Barcelona, Spain

Edited by M. Granger Morgan, Carnegie Mellon University, Pittsburgh, PA, and approved March 25, 2015 (received for review July 13, 2014)

Zoback and Gorelick [(2012) *Proc Natl Acad Sci USA* 109(26):10164–10168] have claimed that geologic carbon storage in deep saline formations is very likely to trigger large induced seismicity, which may damage the caprock and ruin the objective of keeping CO₂ stored deep underground. We argue that felt induced earthquakes due to geologic CO₂ storage are unlikely because (i) sedimentary formations, which are softer than the crystalline basement, are rarely critically stressed; (ii) the least stable situation occurs at the beginning of injection, which makes it easy to control; (iii) CO₂ dissolution into brine may help in reducing overpressure; and (iv) CO₂ will not flow across the caprock because of capillarity, but brine will, which will reduce overpressure further. The latter two mechanisms ensure that overpressures caused by CO₂ injection will dissipate in a moderate time after injection stops, hindering the occurrence of postinjection induced seismicity. Furthermore, even if microseismicity were induced, CO₂ leakage through fault reactivation would be unlikely because the high clay content of caprocks ensures a reduced permeability and increased entry pressure along the localized deformation zone. For these reasons, we contend that properly sited and managed geologic carbon storage in deep saline formations remains a safe option to mitigate anthropogenic climate change.

carbon sequestration | induced seismicity | overpressure | climate change | CO₂ leakage

Zoback and Gorelick (1) claim that geologic carbon storage in deep saline formations is very likely to trigger induced seismicity capable of damaging the caprock, which could ruin the objective of keeping CO₂ stored deep underground. According to them, the main reason for this is that overpressure will be excessively high and failure conditions will be reached because the upper crust is critically stressed, i.e., close to failure. It is true that an excessive overpressure may induce microseismicity and even felt seismicity (2). It is also true that a felt seismic event could stop CO₂ sequestration projects, as happened with the geothermal project Basel Deep Heat Mining Project in Switzerland (3). However, there is no evidence from the existing CO₂ storage projects that CO₂ has the potential of easily inducing large earthquakes (4).

No felt seismic event has been reported to date at either pilot or industrial CO₂ storage projects (4–8). Even at In Salah, Algeria, where a huge overpressure was induced, no felt seismic event has been induced (7, 9). CO₂ storage in depleted gas fields has also been proven to be a safe option both at Otway, Australia (6) and at Lacq, France (5, 8). Actually, CO₂ storage operates under conditions similar to natural gas storage, which has not induced felt seismicity for decades (10–12). The recent induced seismic events at Castor, Spain (13) appears to be the only exception. However, too little is known about this site to extract any lesson. In fact, the very ignorance about what happened at Castor suggests that site understanding and management may be the critical issues.

We argue that large induced earthquakes related to CO₂ injection in deep saline formations are unlikely because (i)

sedimentary formations are rarely critically stressed; (ii) the least stable conditions occur at the beginning of injection; (iii) CO₂ may dissolve at a significant rate, reducing overpressure; and (iv) brine will flow across the caprock, lowering overpressure in the reservoir. For these reasons we believe that geologic carbon storage in deep saline formations remains a safe option for mitigating climate change.

It Is Not True That the Whole Upper Crust Is Critically Stressed

It is generally accepted that the crystalline basement is critically stressed at some depth intervals (14–16). However, CO₂ will be injected in shallow (1–3 km deep) sedimentary formations, which are much softer than the brittle and stiff crystalline basement. As such, stress criticality, i.e., mobilized frictional coefficients, μ , in the range of 0.6–1.0 (17), is not usually observed at shallow depths within sedimentary formations (16, 18–21). We have compiled effective stress data of sedimentary formations and they fall within values of mobilized frictional coefficients around 0.4, i.e., the actual deviatoric stress is lower than the critical one (Fig. 1). This value is moderately low compared with the frictional coefficients around 0.6–0.8 of the critically stressed crystalline basement. In particular, the mobilized friction coefficients of sedimentary rocks where CO₂ is being, has been or is planned to be injected is always lower than the critical value of 0.6. This means that there is a wide margin before CO₂ injection might induce failure conditions and therefore, trigger a seismic event.

To illustrate that sedimentary formations are unlikely to be critically stressed, we have built a simple model of the upper

Significance

Geologic carbon storage remains a safe option to mitigate anthropogenic climate change. Properly sited and managed storage sites are unlikely to induce felt seismicity because (i) sedimentary formations, which are softer than the crystalline basement, are rarely critically stressed; (ii) the least stable situation occurs at the beginning of injection, which makes it easy to control; (iii) CO₂ will dissolve into brine at a significant rate, reducing overpressure; and (iv) CO₂ will not flow across the caprock because of capillarity, but brine will, which will reduce overpressure further. Furthermore, CO₂ leakage through fault reactivation is unlikely because the high clay content of caprocks ensures a reduced permeability and increased entry pressure along localized deformation zones.

Author contributions: V.V. and J.C. designed research; V.V. performed research; V.V. and J.C. analyzed data; and V.V. and J.C. wrote the paper.

The authors declare no conflict of interest.

This article is a PNAS Direct Submission.

¹To whom correspondence should be addressed. Email: victor.vilarrasa@upc.edu.

This article contains supporting information online at www.pnas.org/lookup/suppl/doi:10.1073/pnas.1413284112/-DCSupplemental.

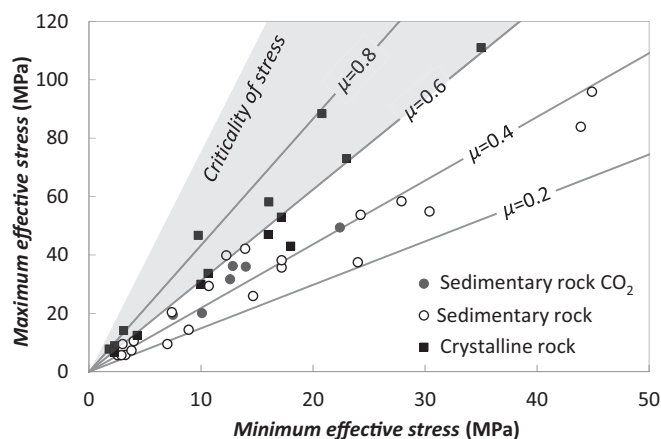


Fig. 1. Maximum versus minimum effective stress measured in wellbores at depth in both crystalline (black squares) and sedimentary rocks (hollow circles). Sedimentary rocks where CO₂ is being, has been or is planned to be injected are marked with black circles. The lines corresponding to several mobilized friction coefficients, μ , are included as a reference. Note that whereas crystalline rocks are critically stressed, sedimentary rocks are usually not.

crust in a typical intraplate setting. The shallowest 2.5 km represent sedimentary rocks and the rest, down to 16 km deep, is crystalline rock. The sedimentary rock is softer than the crystalline rock (see *SI Text* for details). The stress state is initially isotropic, i.e., the mobilized friction coefficient equals 0. We impose a typical intraplate strain rate of 10^{-17} s^{-1} (22). As a result, the crystalline rock becomes critically stressed ($\mu = 0.6$) after 6 Myr. However, the sedimentary rock remains less stressed ($\mu = 0.4$) because of its lower stiffness (Fig. 2). This numerical result is consistent with the low frequency of intraplate seismic events and with the effective stress data compiled in Fig. 1 that evidences that the whole upper crust is not critically stressed. In particular, the shallow ‘soft’ sedimentary formations are far from critically stressed.

Some support for this simple model results from the fact that it yields the maximum mobilized frictional coefficient at a depth between 5 and 6 km (Fig. 2). This means that shallow earthquakes are most likely to occur in the crystalline basement at this depth. Interestingly, this depth of maximum occurrence of earthquakes is consistent with observations of frequency-depth distribution of earthquakes in continental intraplate regions such as Haicheng, China; Thessaloniki, Greece; Hansel Valley, Utah; Pocatello Valley, Idaho; Wasatch, Utah; Coso geothermal field, California (23) and Galicia, Spain (24); and in the plate boundary of the San Andreas Fault, California (23, 25, 26).

The evidence that sedimentary rocks are not critically stressed (Figs. 1 and 2) appears to contradict the large magnitude earthquakes induced by wastewater injection in sedimentary formations in 2011 at Oklahoma, Ohio and Arkansas. These earthquakes have been used as an argument against geologic carbon storage (1). However, the earthquakes were induced in the critically stressed crystalline basement and not in the sedimentary formations where wastewater was injected. Wastewater was injected into the basal aquifer, which led to the pressurization of faults in the crystalline basement (27–29). In the case of the earthquakes of Guy and Greenbrier, Arkansas, wastewater was injected into the Ozark aquifer (3 km deep), which is placed right above the crystalline basement. Wastewater leaked into a deeper fault, inducing four earthquakes of magnitude $M > 3.9$, with a maximum magnitude of 4.7, at around 6 km deep (30). This finding highlights (i) the need for proper characterization and (ii) the importance of a seal below the storage formation, to

isolate the critically stressed crystalline basement from CO₂ injection in sedimentary formations.

It has been conjectured that if an induced earthquake similar to those triggered by wastewater injection in 2011 occurred in a CO₂ storage site, fault reactivation would lead to CO₂ leakage (1). We contend that close analysis of fault zone architecture reveals that CO₂ will not easily penetrate into the portions of the fault contained within shale rocks (31). Fault permeability, which is highly variable in reservoir-caprock sequences (32, 33), decreases several orders of magnitude for increasing clay content, leading to a much lower permeability in the caprocks than in the reservoirs (34, 35). Rocks with low clay content, like reservoirs, tend to fracture, increasing the width of the damaged zone and usually increasing permeability in response to shear (34). However, clay-rich rocks, like caprocks, tend to concentrate shearing in the fault core, which reduces the grain size by friction, thus reducing fault permeability (34). Therefore, shear slip will usually increase fault permeability in the reservoir, but decrease it in the caprock, increasing the permeability contrast in the vertical direction (31, 36). Indeed, numerical simulations show that CO₂ leakage is negligible when accounting for this heterogeneity in permeability in the vertical direction within faults undergoing shear displacement (37). Even assuming constant permeability in the vertical direction within the fault, no correlation has been found between shear slip and CO₂ leakage (38). Furthermore, capillary entry pressure increases with both clay content and reduced pore size, which is what ultimately hinders CO₂ penetration into the fault (39).

Overpressure Evolution

The evolution of overpressure induced by CO₂ injection is significantly different from that of water (or wastewater) injection. Water injection at a constant mass flow rate through a vertical well into an extensive (infinite) confined formation induces an overpressure that increases linearly with the logarithm of time (40). Therefore, overpressure will become large for very long injection times. This was the case at Paradox Valley, Colorado, where overpressure increased more than 16 MPa over a decade of injecting a constant volume of saline water (29). On the other hand, the low viscosity of CO₂ implies that overpressure caused by CO₂ injection peaks at the beginning of injection and drops

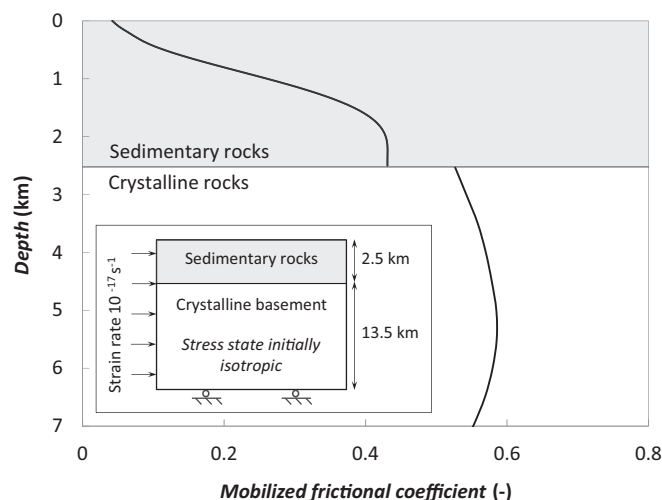


Fig. 2. Mobilized friction coefficient as a function of depth after 6 Myr of applying a strain rate typical of plate tectonics (10^{-17} s^{-1}) in the upper crust considering that the stress field is initially isotropic (see inset for a sketch of the model). Note that whereas the crystalline basement becomes critically stressed, the sedimentary rocks remain far from being critically stressed.

slightly afterward (41–48) (see inlet Fig. 3). This difference makes CO₂ injection particularly interesting because the most critical state occurs at the beginning of injection (41, 49) (Fig. 3). This initial critical situation is illustrated by what happened at Weyburn, Canada, where around 200 microseismic events were induced at the beginning of CO₂ injection, but no more events were measured afterward (50). In fact, initial microseismicity may be reduced by progressively increasing the CO₂ injection rate to avoid the peak in overpressure at the beginning of injection.

Storage formations need not be extensive or fully confined, as assumed in the above discussion. Overpressure induced by CO₂ injection may increase over time if the pressure perturbation cone reaches a flow barrier, such as a low-permeability fault. In such case, or in a compartmentalized reservoir (51), the reservoir storage capacity could be limited by the maximum sustainable injection pressure, defined so as to avoid induced seismicity (52). Fluid pressure must be monitored to identify the presence of flow barriers and to adopt mitigation measures to avoid an excessive overpressure that could lead to induced seismicity and make the operation uneconomical. Nevertheless, the reservoir will never be totally closed and overpressure will dissipate with time, helping to maintain fault stability and hinder postinjection induced earthquakes.

Overpressure will extend tens to hundreds of km for the time scales of CO₂ storage projects, i.e., 30–50 y (53). At these spatial scales, the effective caprock permeability can be two orders of magnitude higher than that of the core scale due to the existence of discontinuities (54). Thus, caprock permeability can become relatively high, i.e., up to 10⁻¹⁶ m² (55). Because the caprock seals brine by permeability, but it seals CO₂ by capillarity, brine, but not CO₂, can flow through the caprock (56). Fig. 4 shows that overpressure can be significantly lowered for relatively permeable caprocks, which would reduce the risk of inducing seismic events through fault reactivation due to the lower overpressure. Furthermore, the lateral extent of the pressure perturbation cone will also be significantly reduced (Fig. 4), which increases the reservoir storage capacity (57) and reduces the number of fractures and faults that will undergo stability changes. Indeed, a steady state could be reached in which the flow rate of brine flowing through the caprock equals the injected flow rate. Using leaky aquifers theory (58), and the geological setting of Fig. 4,

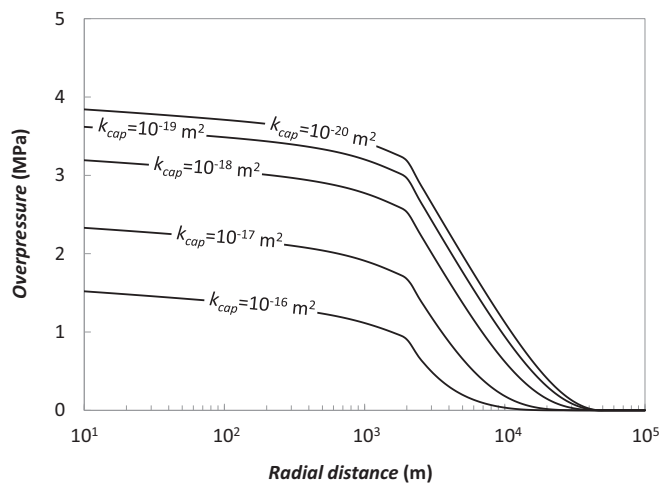


Fig. 4. Radial distribution of the overpressure at the top of the reservoir as a function of the caprock permeability after injecting 2 Mt/y during 2,000 d into a 50-m-thick formation with a permeability of 10⁻¹³ m².

the steady state would be reached after some 200 y of injection if the permeability of the seals is 10⁻¹⁸ m², but only after 21 y if the permeability of the seals equals 10⁻¹⁷ m². Thus, this steady state may take place at some CO₂ injection sites before the injection finishes.

CO₂ Dissolution

CO₂ dissolution reduces the total fluid volume filling the pores, thus reducing overpressure (59) and the risk of induced seismicity. The high solubility of CO₂ makes dissolution one of the main trapping mechanisms in the long term. For instance, it has been observed in carbonate-dominated reservoirs containing naturally occurring CO₂ that up to 90% of this CO₂ can dissolve at the millennial timescale (the remaining 10% would be trapped in precipitated minerals) (60).

CO₂ dissolution also operates over relatively short timescales and provides a significant storage capacity (61, 62). CO₂-rich brine is denser than the native brine, which causes the brine immediately beneath the CO₂ plume to be denser than the brine below. This situation is hydrodynamically unstable and leads to the formation of CO₂-rich gravity fingers that sink to the bottom of the formation and bring fresh brine upwards, forming convective cells that enhance CO₂ dissolution rate (63–67).

CO₂ dissolution is likely to occur quickly for high vertical permeability ($k > 10^{-13}$ m²), which will lower overpressure significantly. Indeed, Elenius et al. (68) calculated that up to 50% of the injected CO₂ at Sleipner ($k = 2 \cdot 10^{-12}$ m²), Norway, becomes rapidly dissolved when the formation brine has no dissolved CO₂. Furthermore, they estimated that between 7 and 26% of the total 15 Mt of CO₂ injected in the period 1996–2011 is already dissolved. These results are in agreement with our calculations (*SI Text*), which predict a dissolution rate at Sleipner of 12% of the injected CO₂. Still, these calculations may underestimate the actual rate at which CO₂ dissolves because they neglect the effect of dispersion, which significantly accelerates the onset of gravitational fingering (64). Furthermore, mass transfer is enhanced by convection in inclined aquifers, which are common in sedimentary basins (69). However, dissolution becomes negligible for low vertical permeability. For instance, at In Salah ($k = 10^{-14}$ m²), Algeria, only 0.03–0.1% of the injected CO₂ dissolves into the brine (68). Therefore, only when vertical permeability is high, CO₂ dissolution will contribute to significantly reduce overpressure with time, progressively leading to a mechanically more stable situation.

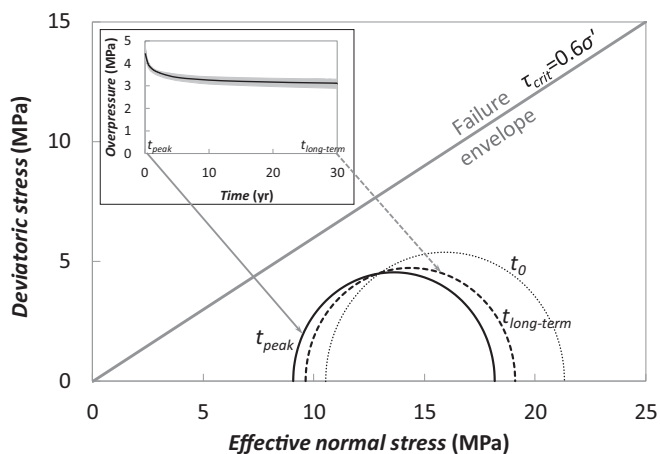


Fig. 3. Caprock stability and overpressure evolution in the reservoir at the injection well when injecting a constant mass flow rate of CO₂ (2 Mt/y) through a vertical well. The shadowed region in the inlet indicates the range of overpressures calculated by varying hydromechanical properties. Note that, initially, the stress state is far from failure conditions and that the less stable conditions occur at the beginning of injection.

Discussion and Conclusions

We have given evidence that sedimentary formations are not, in general, critically stressed (recall Figs. 1 and 2). Furthermore, overpressure will be relatively small when injecting CO₂ because (i) it peaks at the beginning of injection and afterward drops slightly (recall Fig. 3); (ii) CO₂ dissolution may occur quickly and at a significant rate, if the vertical permeability of the reservoir is high, contributing to reduce overpressure; and (iii) because brine, but not CO₂ because of capillarity, can flow through the caprock, overpressure will be lowered significantly and a steady state may be reached at some sites within the injection period (recall Fig. 4). The combined effect of a noncritically stressed storage formation and a small overpressure make geologic storage a safe strategy to reduce emissions of greenhouse gasses to the atmosphere.

This conclusion is not meant as an unqualified approval of any site for storage. Every site requires a proper suitability study. To this end, numerous best practices manuals are available (see ref. 70 for a review). The key issue is site characterization (71), which includes proper structural geology understanding and a good hydromechanical testing (72). Characterization may lead to dismissal of some reservoirs. Still, the point is that suitable sedimentary basins to store huge volumes of CO₂ are abundant around the world (62, 73, 74).

Experience with CO₂ storage is still limited, so few generalizations can be made. Instead, some lessons can be learnt from geothermal operations, despite the fact that these tend to concentrate in regions of anomalous thermal gradients, which are more prone to instability. For instance, fluid injection in sedimentary rocks within the overpressure ranges that are reasonable for CO₂ injection, i.e., $\Delta P < 10$ MPa, do not usually induce seismicity (3 sites with seismic events greater than magnitude 2 out of 23 injection sites reviewed by ref. 16). Induced seismicity is much more likely in crystalline rocks (3 sites with seismic events greater than M 1.9 out of 3 injection sites in granites when the injection pressure was lower or equal than 11 MPa) (16). These data confirm that, contrary to crystalline rocks, sedimentary rocks are rarely critically stressed (recall Figs. 1 and 2).

Natural seismicity should also be considered in site selection (74). Fluid injections at European sites with low natural seismicity have not produced felt events (16). Acknowledging that earthquake frequency tends to peak at plate boundaries (75, 76) further supports the suitability of most sedimentary basins due to their low natural seismicity. Furthermore, earthquake magnitude increases with depth (77–83) and therefore, large induced earthquakes (M > 4) that might jeopardize the caprock sealing capacity are unlikely to be triggered at the shallow depths at which CO₂ will be injected (recall Fig. 2).

In addition to a proper site characterization, overpressure management will contribute to avoid felt induced earthquakes

(52, 84), as proposed by Zoback (85) for wastewater disposal. Numerical simulations have shown that CO₂ injection in closed reservoirs without a proper control of overpressure, i.e., allowing overpressure to exceed the maximum sustainable injection pressure, has the potential of triggering earthquakes of up to magnitude 4.5 in critically stressed faults (86). However, the magnitude of the simulated induced earthquakes becomes smaller than 3 when considering more realistic stress fields for sedimentary formations, with shear displacements of up to 6 cm (86, 87). These numerical studies highlight the importance of overpressure management for avoiding felt induced seismicity.

Even if a seism of sufficient magnitude occurs, CO₂ may not necessarily leak because fault permeability is reduced and entry pressure increased in faults across rocks containing clay (37). Moreover, a self-healing mechanism that prevents CO₂ leakage has been observed in argillaceous limestones (88). We conjecture that these mechanisms, together with increased buoyancy, may explain why CO₂ natural analogs often leak at shallow depths (less than 700 m, where CO₂ is gaseous), but deep natural CO₂ deposits rarely do (89).

Coupled thermo-mechanical effects also deserve attention. CO₂ will generally reach the storage formation at a temperature lower than that of the rock (90). In fact, injecting liquid (cold) CO₂ and maintaining liquid conditions along the wellbore is energetically advantageous (and therefore, it is likely to become a common practice) because it significantly reduces compression costs (91). Cold injection will cause a cold region around the injection well, which will induce thermal stress reduction. This stress reduction may lead to fracture instabilities within the reservoir (92), where induced microseismicity may be beneficial as it enhances injectivity. However, cold CO₂ injection improves caprock stability in normal faulting stress regimes because the caprock tightens as a result of stress redistribution, even in the presence of stiff caprocks (93). Thus, injection of cold CO₂ should further improve stability in tectonically stable regions.

Zoback and Gorelick (1) concluded that large-scale geologic carbon storage will be extremely expensive and risky. Economic issues fall beyond our expertise and the scope of this review (but it seems evident that economic feasibility will depend on the prize of CO₂ emissions). However, we have provided abundant evidence to state that large-scale CO₂ storage is not risky and, thus, will be a safe option to mitigate anthropogenic climate change.

ACKNOWLEDGMENTS. This work was funded by the Assistant Secretary for Fossil Energy, Office of Natural Gas and Petroleum Technology, through the National Energy Technology Laboratory under US Department of Energy Contract DE-AC02-05CH11231. This work was supported by the “TRUST” (trust-co2.org) and “PANACEA” (www.panacea-co2.org) projects (from the European Community’s Seventh Framework Programme FP7/2007-2013 Grants 309607 and 282900, respectively).

- Zoback MD, Gorelick SM (2012) Earthquake triggering and large-scale geologic storage of carbon dioxide. *Proc Natl Acad Sci USA* 109(26):10164–10168.
- Hsieh PA, Bredehoeft JD (1981) A reservoir analysis of the Denver earthquakes: A case of induced seismicity. *J Geophys Res* 86(B2):903–920.
- Håring MO, Schanz U, Ladner F, Dyer BC (2008) Characterization of the Basel 1 enhanced geothermal system. *Geothermics* 37:469–495.
- IEAGHG (2013) *Induced Seismicity and Its Implications for CO₂ Storage Risk*. Report 2013/09, (International Energy Agency Greenhouse Gas R&D Program (IEAGHG), Cheltenham, UK).
- Lescanne M, Hy-Billiot J, Aimard N, Prinset C (2011) The site monitoring of the Lacq industrial CCS reference project. *Energy Procedia* 4:3518–1525.
- Jenkins CR, et al. (2012) Safe storage and effective monitoring of CO₂ in depleted gas fields. *Proc Natl Acad Sci USA* 109(2):E35–E41.
- Rutqvist J (2012) The geomechanics of CO₂ storage in deep sedimentary formations. *International Journal of Geotechnical and Geological Engineering* 30:525–551.
- Prinset C, Thibeau S, Lescanne M, Monne J (2013) Lacq-Rousse CO₂ capture and storage demonstration pilot: Lessons learnt from two and a half years monitoring. *Energy Procedia* 37:3610–3620.
- Gemmer L, Hansen O, Iding M, Leary S, Ringrose P (2012) Geomechanical response to CO₂ injection at Krechba, In Salah, Algeria. *First Break* 30(2):79–84.
- Nagelhout ACG, Roest JPA (1997) Investigating fault slip in a model of underground gas storage facility. *Int J Rock Mechanics, Mining Sci Geomechanical Abstr* 34:212.
- Rutqvist J, Stephansson O (2003) The role of hydromechanical coupling in fractured rock engineering. *Hydrogeol J* 11:7–40.
- Teatini P, et al. (2011) Geomechanical response to seasonal gas storage in depleted reservoirs: A case study in the Po River basin, Italy. *J Geophys Res* 116:F02002.
- Cesca S, et al. (2014) The 2013 September–October seismic sequence offshore Spain: A case of seismicity triggered by gas injection? *Geophys J Int* 198:941–953.
- Cornet FH, Jianmin Y (1995) Analysis of induced seismicity for stress field determination and pore pressure mapping. *Pure Appl Geophys* 145:677–700.
- Townend J, Zoback MD (2000) How faulting keeps the crust strong. *Geology* 28(5):399–402.
- Evans KF, Zappone A, Kraft T, Deichmann N, Moia F (2012) A survey of the induced seismic responses to fluid injection in geothermal and CO₂ reservoirs in Europe. *Geothermics* 41:30–54.
- Byerlee JD (1978) Friction of rocks. *Pure Appl Geophys* 116:615–629.
- Haimson BC (1977) Crustal stress in the continental United States as derived from hydrofracturing tests. *Geophysical Monograph Series* 20:576–592.
- McGarr A, Gay NC (1978) State of stress in the earth’s crust. *Annu Rev Earth Planet Sci* 6:405–436.

20. Dahm T, et al. (2010) How to discriminate induced, triggered and natural seismicity. *Proceedings of the Workshop Induced Seismicity*, eds Ritter J, Oth A (Centre Européen de Géodynamique et de Séismologie, Luxembourg), Vol 30, pp 69–76.
21. Gunzburger Y (2010) Stress state interpretation in light of pressure-solution creep: Numerical modelling of limestone in the Eastern Paris Basin, France. *Tectonophysics* 483(3):377–389.
22. Zoback MD, Townend J, Grollmund B (2002) Steady-state failure equilibrium and deformation of intraplate lithosphere. *Int Geol Rev* 44:383–401.
23. Meissner R, Strehlau J (1982) Limits of stresses in continental crusts and their relation to the depth-frequency distribution of shallow earthquakes. *Tectonics* 1:73–89.
24. Martin-Gonzalez F, et al. (2012) Seismicity and potentially active faults in the Northwest and Central-West Iberian Peninsula. *Journal of Iberian Geology* 38:52–69.
25. Tse ST, Rice JR (1986) Crustal earthquake instability in relation to the depth variation of frictional slip properties. *J Geophys Res* 91:9452–9472.
26. Magistrale H, Zhou H (1996) Lithologic control of the depth of earthquakes in Southern California. *Science* 273(5275):639–642.
27. Keranen KM, Savage HM, Abers GA, Cochran ES (2013) Potentially induced earthquakes in Oklahoma, USA: Links between wastewater injection and the 2011 Mw 5.7 earthquake sequence. *Geology* 41(6):699–702.
28. Zhang Y, et al. (2013) Hydrogeologic controls on induced seismicity in crystalline basement rocks due to fluid injection into basal reservoirs. *Ground Water* 51(4):525–538.
29. Ellsworth WL (2013) Injection-induced earthquakes. *Science* 341(6142):1225942.
30. Kerr RA (2012) Seismology. Learning how to not make your own earthquakes. *Science* 335(6075):1436–1437.
31. Caine JS, Evans JP, Forster CB (1996) Fault zone architecture and permeability structure. *Geology* 24(11):1025–1028.
32. Takahashi M (2003) Permeability change during experimental fault smearing. *J Geophys Res Solid Earth* 108(B5):2235.
33. Egholm DL, Clausen OR, Sandiford M, Kristensen MB, Korstgård JA (2008) The mechanics of clay smearing along faults. *Geology* 36(10):787–790.
34. Bense VF, Person MA (2006) Faults as conduit - barrier systems to fluid flow in siliciclastic sedimentary aquifers. *Water Resour Res* 42:W05421.
35. Crawford BR, Faulkner DR, Rutter EH (2008) Strength, porosity, and permeability development during hydrostatic and shear loading of synthetic quartz-clay fault gouge. *J Geophys Res Solid Earth* 113:B03207.
36. Weber K, Mandl G, Pilar WF, Lehner F, Precious RG (1978) The role of faults in hydrocarbon migration and trapping in Nigeria growth fault structures. *Offshore Technology Conference* 10:2643–2653.
37. Rinaldi AP, Jeanne P, Rutqvist J, Cappa F, Guglielmi Y (2014) Effects of fault-zone architecture on earthquake magnitude and gas leakage related to CO₂ injection in a multi-layered sedimentary system. *Greenhouse Gases: Science and Technology* 4:99–120.
38. Rinaldi AP, Rutqvist J, Cappa F (2014) Geomechanical effects on CO₂ leakage through fault zones during large-scale underground injection. *Int J Greenh Gas Control* 20:117–131.
39. Manzcocci T, Childs C, Walsh JJ (2010) Faults and fault properties in hydrocarbon flow models. *Geofluids* 10:94–113.
40. Cooper HH, Jacob CE (1946) A generalized graphical method for evaluating formation constants and summarizing well field history. *Am Geophys Union Trans* 27:526–534.
41. Vilarrasa V, Bolster D, Olivella S, Carrera J (2010) Coupled hydromechanical modeling of CO₂ sequestration in deep saline aquifers. *Int J Greenh Gas Control* 4:910–919.
42. Hennings J, et al.; CO₂SINK Group (2011) P-T-p and two-phase fluid conditions with inverted density profile in observation wells at the CO₂ storage site at Ketzin (Germany). *Energy Procedia* 4:6085–6090.
43. Okwen RT, Stewart MT, Cunningham JA (2011) Temporal variations in near-wellbore pressures during CO₂ injection in saline aquifers. *Int J Greenh Gas Control* 5:1140–1148.
44. Zhang Z, Agarwal RK (2012) Numerical simulation and optimization of CO₂ sequestration in saline aquifers for vertical and horizontal well injection. *Comput Geosci* 16:891–899.
45. Martens S, et al.; The Ketzin Group (2012) Europe's longest-operating on-shore CO₂ storage site at Ketzin, Germany: A progress report after three years of injection. *Environmental Earth Sciences* 67:323–334.
46. Vilarrasa V, Carrera J, Bolster D, Dentz M (2013) Semianalytical solution for CO₂ plume shape and pressure evolution during CO₂ injection in deep saline formations. *Transp Porous Media* 97:43–65.
47. Martinez MJ, Newell P, Bishop JE, Turner DZ (2013) Coupled multiphase flow and geomechanics model for analysis of joint reactivation during CO₂ sequestration operations. *Int J Greenh Gas Control* 17:148–160.
48. Vilarrasa V (2014) Impact of CO₂ injection through horizontal and vertical wells on the caprock mechanical stability. *Int J Rock Mech Min Sci* 66:151–159.
49. Yamamoto S, Miyoshi S, Sato S, Suzuki K (2013) Study on geomechanical stability of the aquifer-caprock system during CO₂ sequestration by coupled hydromechanical modelling. *Energy Procedia* 37:3989–3996.
50. Verdon JP, Kendall J-M, White DJ, Angus DA (2011) Linking microseismic event observations with geomechanical models to minimise the risks of storing CO₂ in geological formations. *Earth Planet Sci Lett* 305:143–152.
51. Castelletto N, Gambolati G, Teatini P (2013) Geological CO₂ sequestration in multi-compartment reservoirs: Geomechanical challenges. *J Geophys Res Solid Earth* 118(5):2417–2428.
52. Rutqvist J, Birkholzer JT, Cappa F, Tsang C-F (2007) Estimating maximum sustainable injection pressure during geological sequestration of CO₂ using coupled fluid flow and geomechanical fault-slip analysis. *Energy Convers Manage* 48:1798–1807.
53. Birkholzer JT, Zhou Q (2009) Basin-scale hydrogeologic impacts of CO₂ storage: Capacity and regulatory implications. *Int J Greenh Gas Control* 3:745–756.
54. Neuzil CE (1986) Groundwater flow in low-permeability environments. *Water Resour Res* 22(8):1163–1195.
55. Neuzil CE (1994) How permeable are clays and shales? *Water Resour Res* 30(2):145–150.
56. Birkholzer JT, Zhou Q, Tsang C-F (2009) Large-scale impact of CO₂ storage in deep saline aquifers: A sensitivity study on pressure response in stratified systems. *Int J Greenh Gas Control* 3:181–194.
57. Chang KW, Hesse MA, Nicot JP (2013) Reduction of lateral pressure propagation due to dissipation into ambient mudrocks during geological carbon dioxide storage. *Water Resour Res* 49(5):2573–2588.
58. Hantush MS (1960) Modification of the theory of leaky aquifers. *J Geophys Res* 65(11):3713–3725.
59. Mathias SA, Gluyas JG, Gonzalez Martinez de Miguel GJ, Hosseini SA (2011) Role of partial miscibility on pressure buildup due to constant rate injection of CO₂ into closed and open brine aquifers. *Water Resour Res* 47:W12525.
60. Giffillan SM, et al. (2009) Solubility trapping in formation water as dominant CO₂ sink in natural gas fields. *Nature* 458(7238):614–618.
61. MacMinn CW, Szulczewski ML, Juanes R (2011) CO₂ migration in saline aquifers. Part2. Capillary and solubility trapping. *J Fluid Mech* 688:321–351.
62. Szulczewski ML, MacMinn CW, Herzog HJ, Juanes R (2012) Lifetime of carbon capture and storage as a climate-change mitigation technology. *Proc Natl Acad Sci USA* 109(14):5185–5189.
63. Riaz A, Hesse MA, Tchelepi HA, Orr FM, Jr (2006) Onset of convection in a gravitationally unstable boundary layer in porous media. *J Fluid Mech* 548:87–111.
64. Hidalgo JJ, Carrera J (2009) Effect of dispersion on the onset of convection during CO₂ sequestration. *J Fluid Mech* 640:441–452.
65. Neufeld JA, et al. (2010) Convective dissolution of carbon dioxide in saline aquifers. *Geophys Res Lett* 37:L22404.
66. Pau GSH, et al. (2010) High resolution simulation and characterization of density-driven flow in CO₂ storage in saline aquifers. *Adv Water Resour* 33(4):443–455.
67. Elenius MT, Johannsen K (2012) On the time scales of nonlinear instability in miscible displacement porous media flow. *Comput Geosci* 16:901–911.
68. Elenius MT, Nordbotten JM, Kalisch H (2012) Effects of a capillary transition zone on the stability of a diffusive boundary layer. *IMA J Appl Math* 77:771–787.
69. Tsai PA, Riesing K, Stone HA (2013) Density-driven convection enhanced by an inclined boundary: Implications for geological CO₂ storage. *Phys Rev E Stat Nonlin Soft Matter Phys* 87(1):011003.
70. CO₂CRC (Cooperative Research Centre for Greenhouse Gas Technologies) (2011) *A Review of Existing Best Practice Manuals for Carbon Dioxide Storage and Regulation: A Desktop Study Prepared for the Global CCS Institute*, (Cooperative Research Centre for Greenhouse Gas Technologies, Canberra, Australia).
71. Juanes R, Hager BH, Herzog HJ (2012) No geologic evidence that seismicity causes fault leakage that would render large-scale carbon capture and storage unsuccessful. *Proc Natl Acad Sci USA* 109(52):E3623–E3623, author reply E3624.
72. Vilarrasa V, Carrera J, Olivella S (2013) Hydromechanical characterization of CO₂ injection sites. *Int J Greenh Gas Control* 19:665–677.
73. Hitchon B, Gunter WD, Gentzis T, Bailey RT (1999) Sedimentary basins and greenhouse gases: A serendipitous association. *Energy Convers Manage* 40:825–843.
74. Bachu S (2003) Screening and ranking of sedimentary basins for sequestration of CO₂ in geological media in response to climate change. *Environmental Geology* 44:277–289.
75. Stein S, Wyssession M (2003) *An Introduction to Seismology, Earthquakes, and Earth Structure* (Blackwell, Oxford).
76. Kanamori H, Brodsky EE (2004) The physics of earthquakes. *Rep Prog Phys* 67:1429–1496.
77. Scholz CH (1968) The frequency-magnitude relation of microfracturing in rock and its relation to earthquakes. *Bull Seismol Soc Am* 58(1):399–415.
78. Raleigh CB, Healy JH, Bredehoeft JD (1976) An experiment in earthquake control at Rangely, Colorado. *Science* 191(4233):1230–1237.
79. Das S, Scholz CH (1983) Why large earthquakes do not nucleate at shallow depths. *Nature* 305:621–623.
80. Scholz CH (1988) The critical slip distance for seismic faulting. *Nature* 336:761–763.
81. Mori J, Abercrombie RE (1997) Depth dependence of earthquake frequency - magnitude distributions in California: Implications for rupture initiation. *J Geophys Res Solid Earth* 102(B7):15081–15090.
82. Majer EL, et al. (2007) Induced seismicity associated with enhanced geothermal systems. *Geothermics* 36(3):185–222.
83. Yang W, Hauksson E (2011) Evidence for vertical partitioning of strike-slip and compressional tectonics from seismicity, focal mechanisms, and stress drops in the east Los Angeles basin area, California. *Bull Seismol Soc Am* 101(3):964–974.
84. Streit JE, Hillis RR (2004) Estimating fault stability and sustainable fluid pressures for underground storage of CO₂ in porous rock. *Energy* 29:1445–1456.
85. Zoback MD (2012) Managing the seismic risk posed by wastewater disposal. *Earth Magazine* 57(4):38–42.
86. Cappa F, Rutqvist J (2011) Impact of CO₂ geological sequestration on the nucleation of earthquakes. *Geophys Res Lett* 38:L17313.
87. Mazzoldi A, Rinaldi AP, Borgia A, Rutqvist J (2012) Induced seismicity within geologic carbon sequestration projects: Maximum earthquake magnitude and leakage potential. *Int J Greenh Gas Control* 10:434–442.
88. Noiriél C, Made B, Gouze P (2007) Impact of coating development on the hydraulic and transport properties of argillaceous limestone fractures. *Water Resour Res* 43:W09406.

89. Miocic JM, Gilfillan S, McDermott C, Haszeldine RS (2013) Mechanisms for CO₂ leakage prevention—A global dataset of natural analogues. *Energy Procedia* 40: 320–328.
90. Paterson L, Lu M, Connell LD, Ennis-King J (2008) Numerical modeling of pressure and temperature profiles including phase transitions in carbon dioxide wells. *SPE Annual Technical Conference and Exhibition*, September 21–24, 2008, Paper SPE 115946, (Society of Petroleum Engineers (SPE), Denver).
91. Vilarrasa V, Silva O, Carrera J, Olivella S (2013) Liquid CO₂ injection for geological storage in deep saline aquifers. *Int J Greenh Gas Control* 14:84–96.
92. de Simone S, Vilarrasa V, Carrera J, Alcolea A, Meier P (2013) Thermal coupling may control mechanical stability of geothermal reservoirs during cold water injection. *Phys Chem Earth* 64:117–126.
93. Vilarrasa V, Olivella S, Carrera J, Rutqvist J (2014) Long term impacts of cold CO₂ injection on the caprock integrity. *Int J Greenh Gas Control* 24:1–13.