



**Hampton Roads Sanitation District
(HRSD)**

Virginia Beach, VA

**Sustainable Water Initiative for
Tomorrow (SWIFT)**

**Managed Aquifer Recharge (MAR)
Program**

**“MAR Well Design for a Challenging
Environment”**

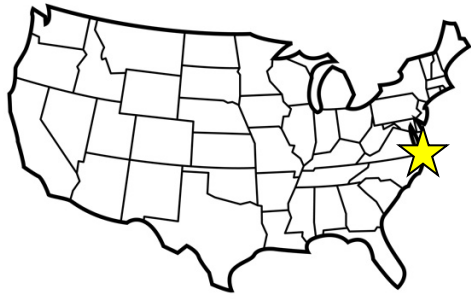
Presented to



Annual Forum

Sept. 12-14, 2023

Tampa, FL



Population served: 1.9 million
14th Largest Wastewater Utility



Political Subdivision created in 1940
Serves 20 Cities and Counties



Combined wastewater treatment capacity: 225 million gallons/day

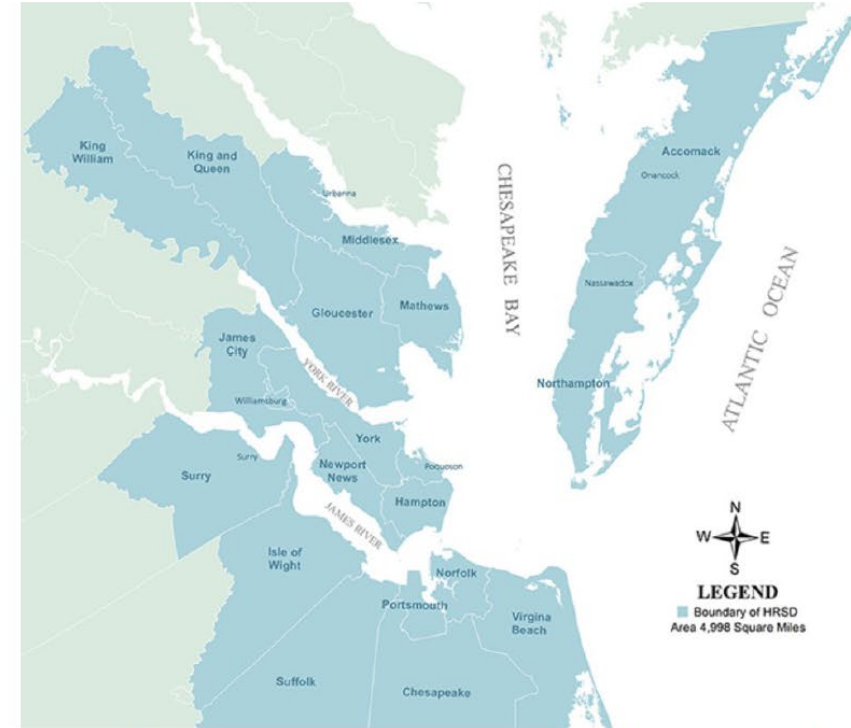


Operate 8 major and 6 smaller treatment plants and more than 100 pump stations



Separate Sanitary System with > 500 miles of pipe

About Us



Service area is approx. 5,000 square miles

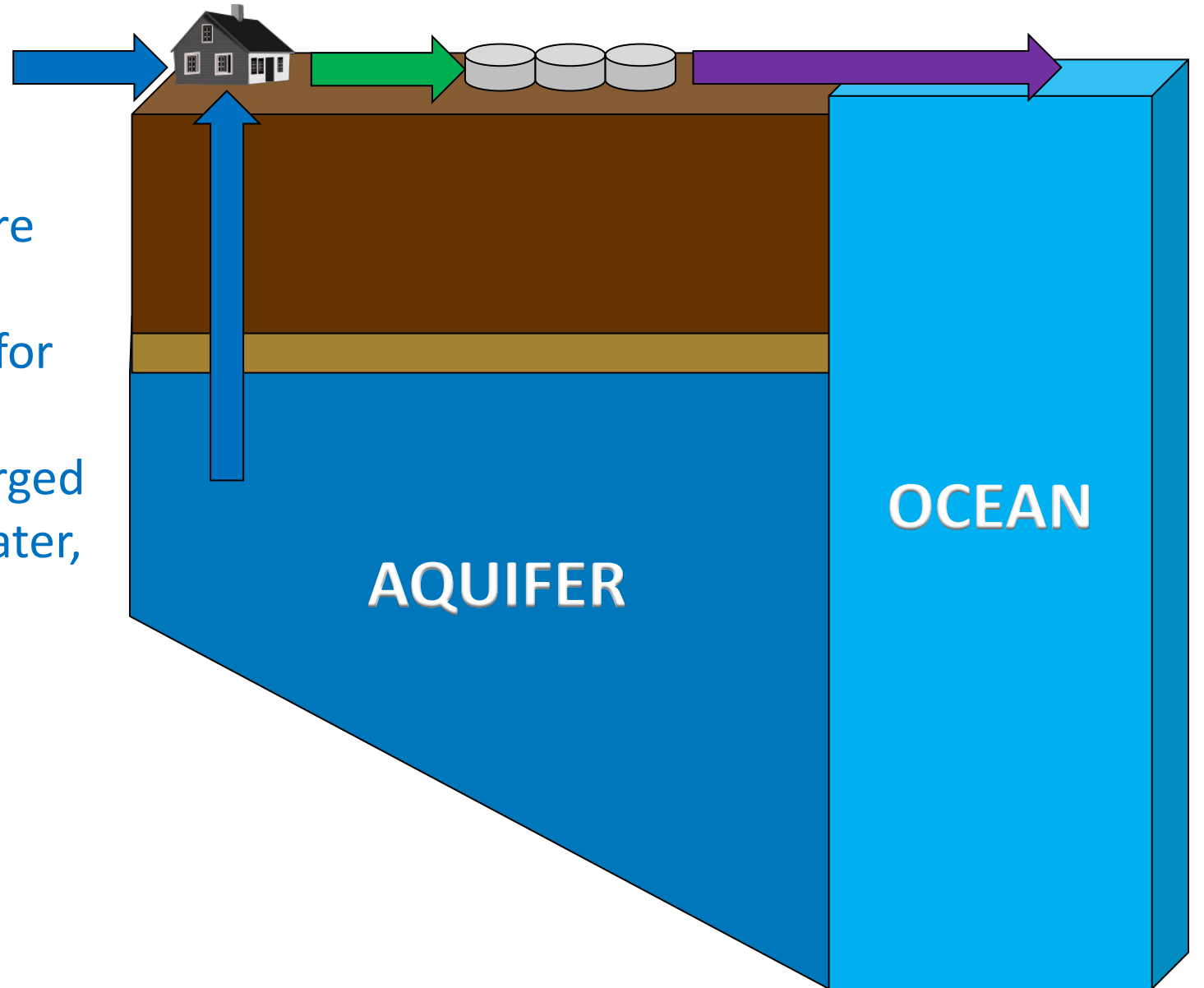
Water challenges

- Restoration of the Chesapeake Bay
 - **Nutrient loading**
 - Harmful Algal Blooms
 - Localized bacteria impairments
 - Urban stormwater retrofits (cost and complexity)
- Adaptation to sea level rise
 - Recurrent flooding
 - **Land subsidence**
- Depletion of groundwater resources
 - **Including potential for saltwater contamination**
- Wet weather sewer overflows
 - Compliance with Federal enforcement action



Currently...

- Surface water and groundwater are consumed
- Wastewater is conveyed to HRSD for treatment
- Highly treated wastewater discharged to lower Chesapeake Bay – salt water, tidal with flow to Atlantic – no downstream users



The future...SWIFT

Treat water to meet drinking water standards and replenish the aquifer with clean water to:

- Provide regulatory stability for wastewater treatment
- Reduce nutrient discharges to the Bay
- Provide a sustainable supply of groundwater
- Reduce the rate of land subsidence
- Protect the groundwater from saltwater contamination

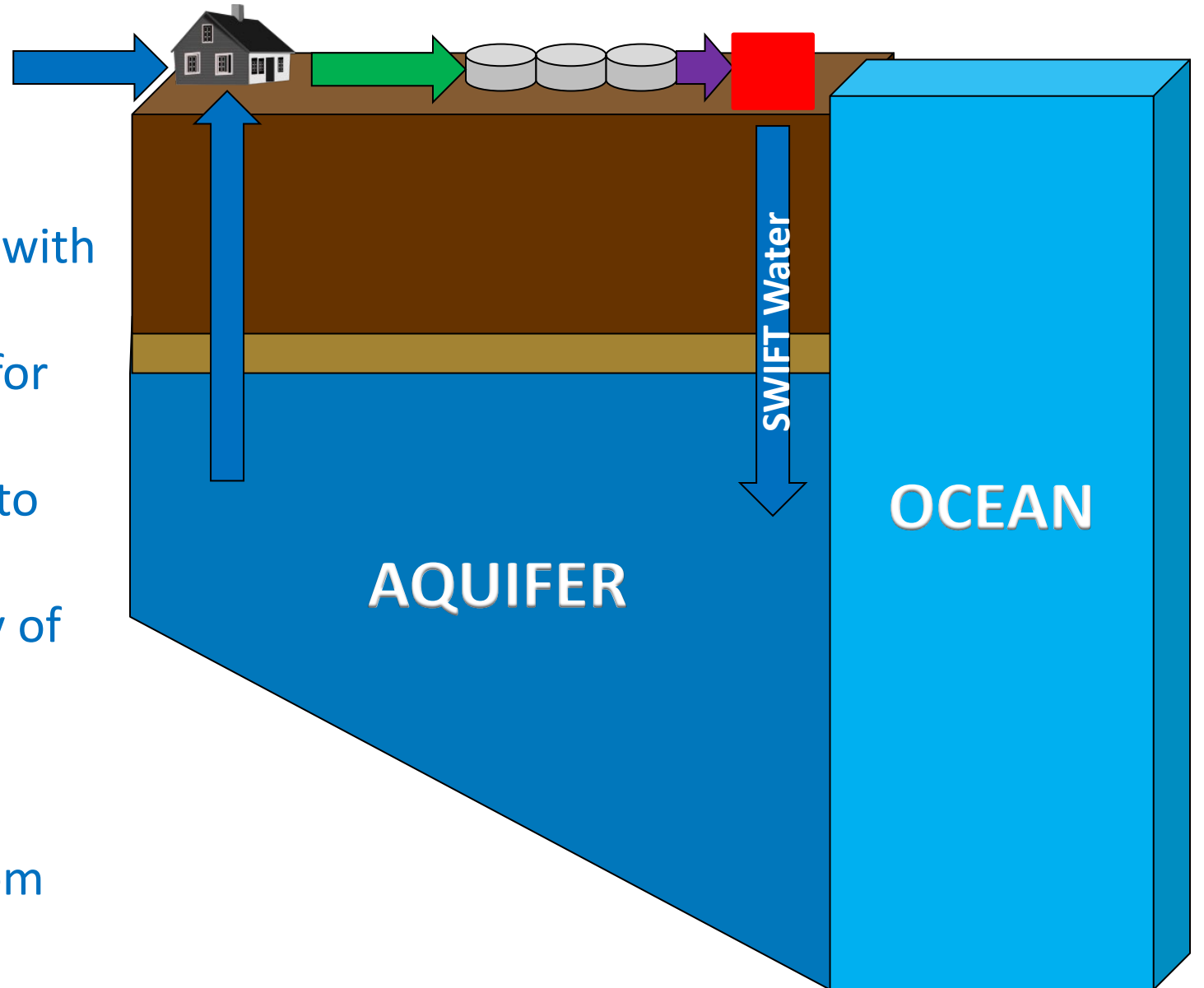
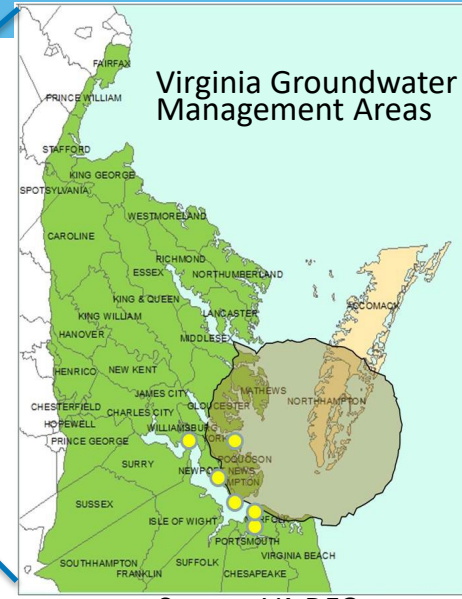
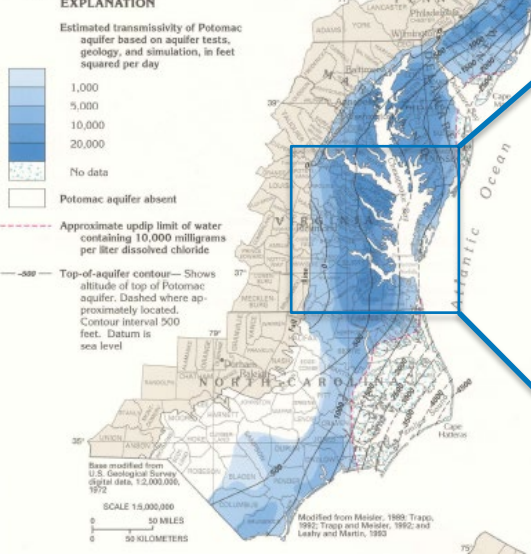
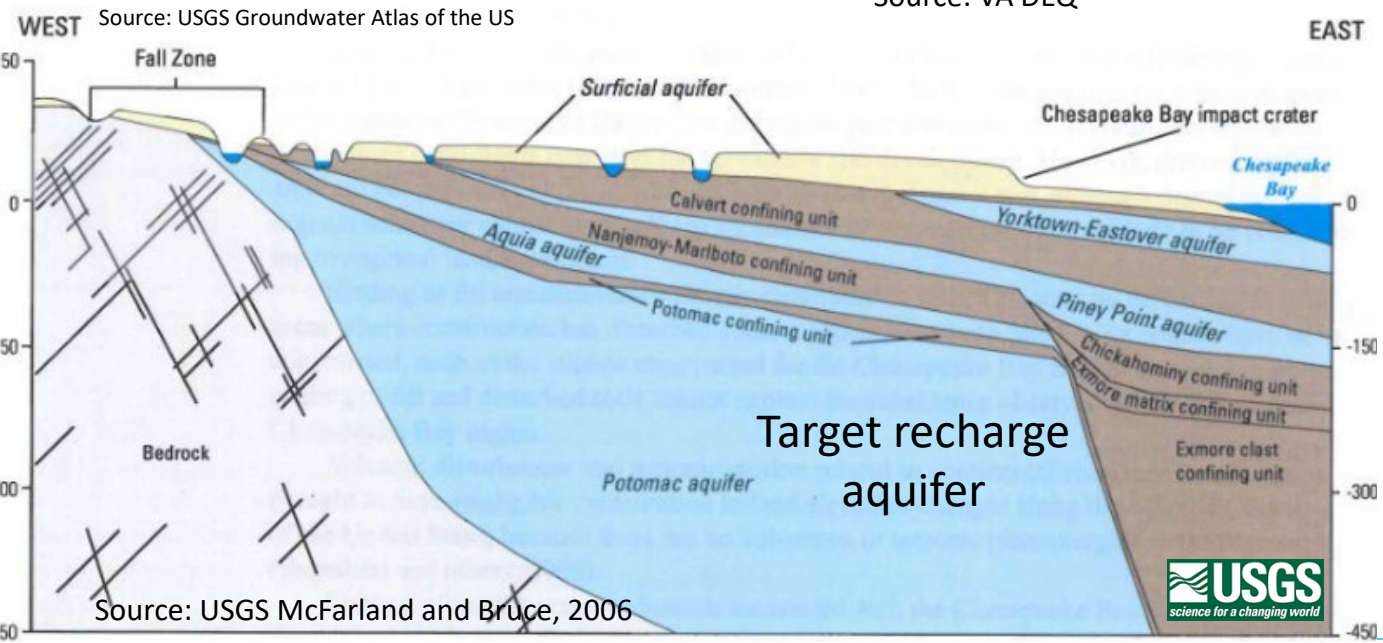


Figure 54. The top of the Potomac aquifer is above sea level along its western and northwestern limit from northernmost North Carolina to New Jersey but slopes to more than 2,500 feet below sea level along the coast of New Jersey and to more than 4,500 feet below sea level near Cape Hatteras in easternmost North Carolina. The transmissivity of the aquifer is highest near Chesapeake Bay and in central New Jersey.



VA Coastal Plain Aquifer System Geometry

- Fall Zone to the Ocean
- Horizontally stacked aquifers = confined aquifers
- Wedge shaped that widens and dips toward the east
- 2,000 feet of unconsolidated sediments (gravels, sands, silts, clays, shells).
- Potomac aquifer, thick and highly interbedded



Well Design Drivers

- **MAR Wells**

- design recharge and backflush rates and related well levels
- anticipated casing and screen depths
- filter pack stability and maintenance
- recharge zone groundwater quality and static pressures
- Native GW and SWIFT water quality

- **Monitoring Wells**

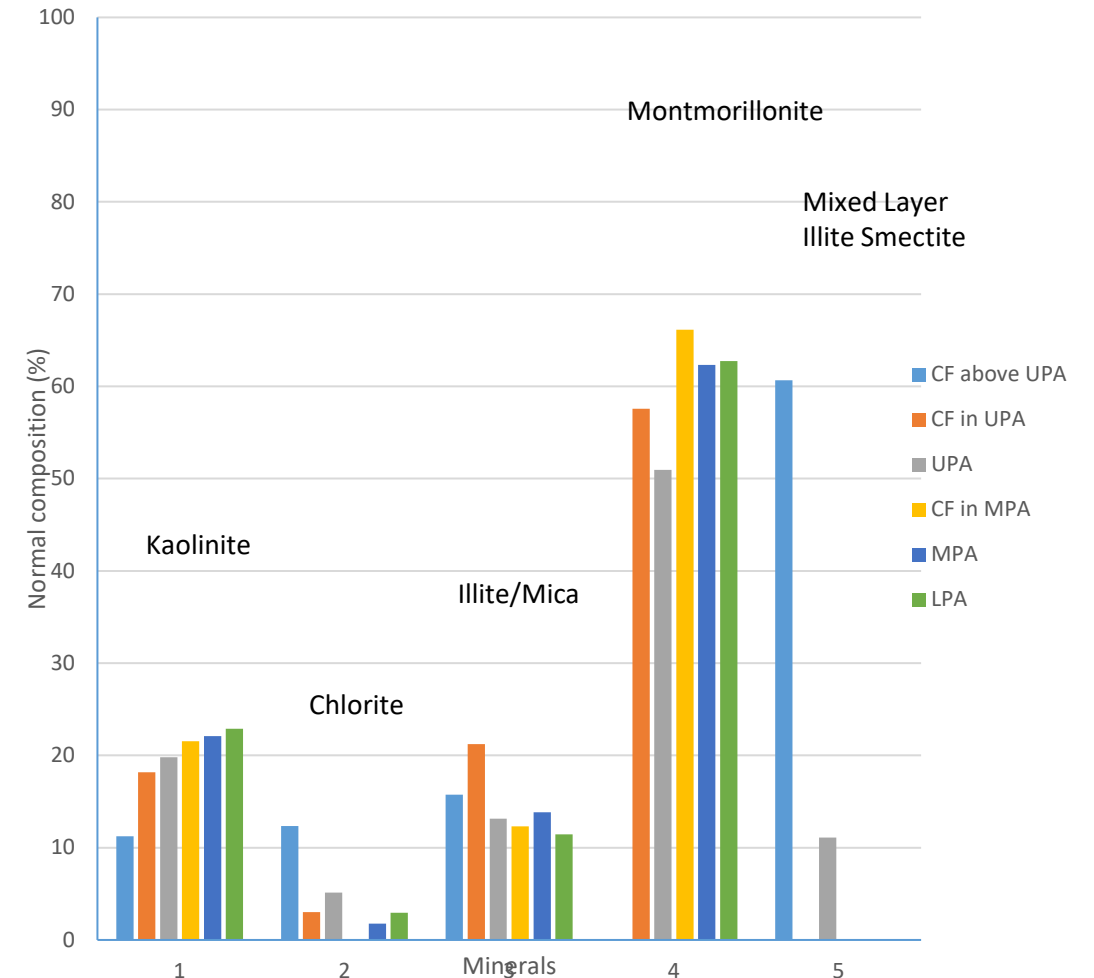
- design purge rates and related well levels
- anticipated casing and screen depths
- recharge zone groundwater quality and static pressures
- Native GW and SWIFT water quality



Well Design Drivers (Cont'd)

- Schedule constraints
 - JRTP MAR wells constructed in two phases
 - Phase 1 (on-site) 3 MAR wells
 - Phase 2 (off-site) 7 MAR wells
 - Based on availability of drilling locations and desire to minimize conflicts with design-build contractor
 - Phase 1 MAR wells (on-site) could sit idle up to 4 years
- Recharge zone plugging
 - SWIFT water significantly lower ionic strength than Native GW
 - clay minerals present in the matrix pores

Clay Mineral Species Abundance

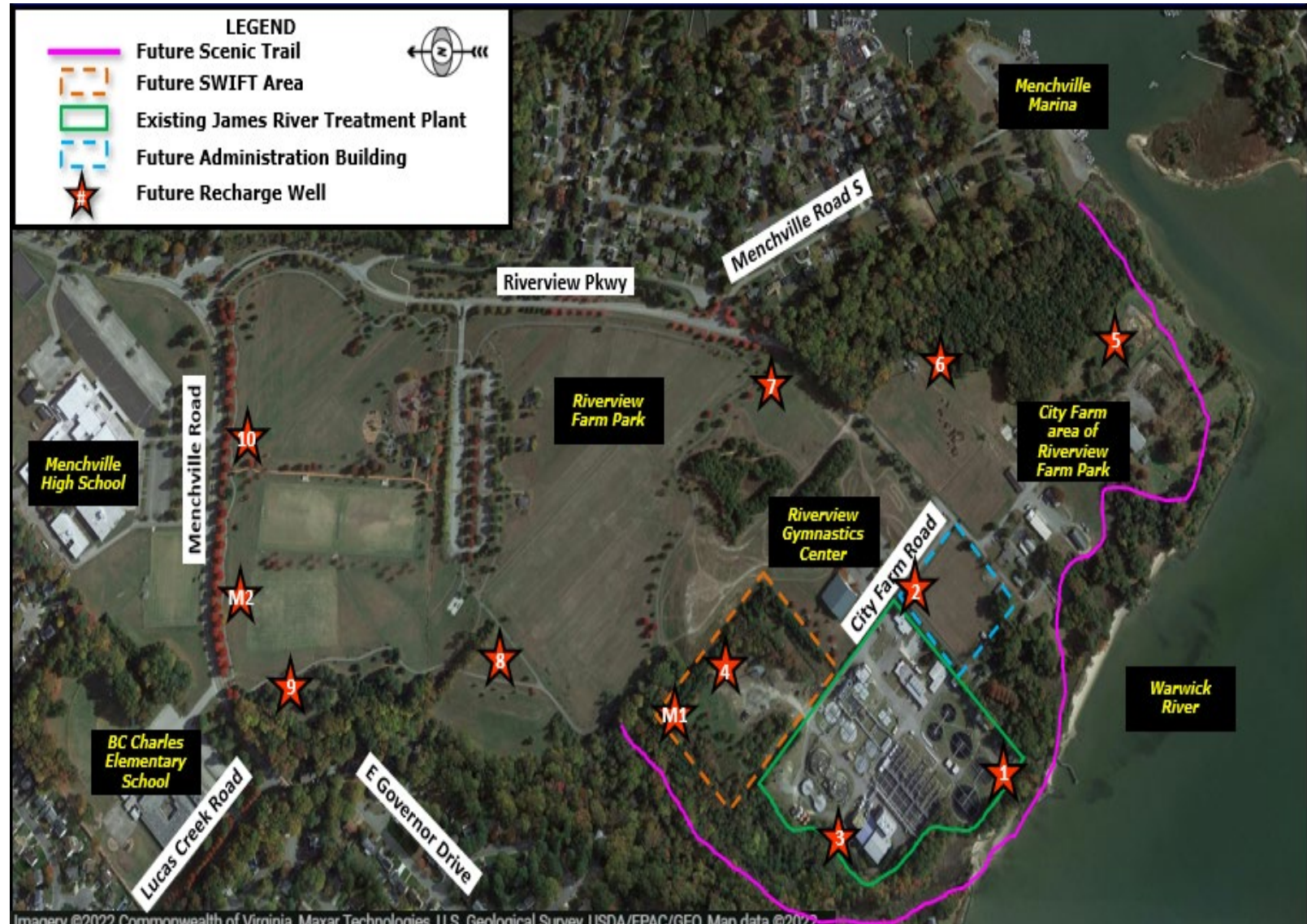


James River Wastewater Treatment Plant (JRTP) is site of first MAR well construction project

- 2 Contracts

- On-Site = 3 MAR wells

- Off-Site = 7 MAR wells + 1 monitoring well nest

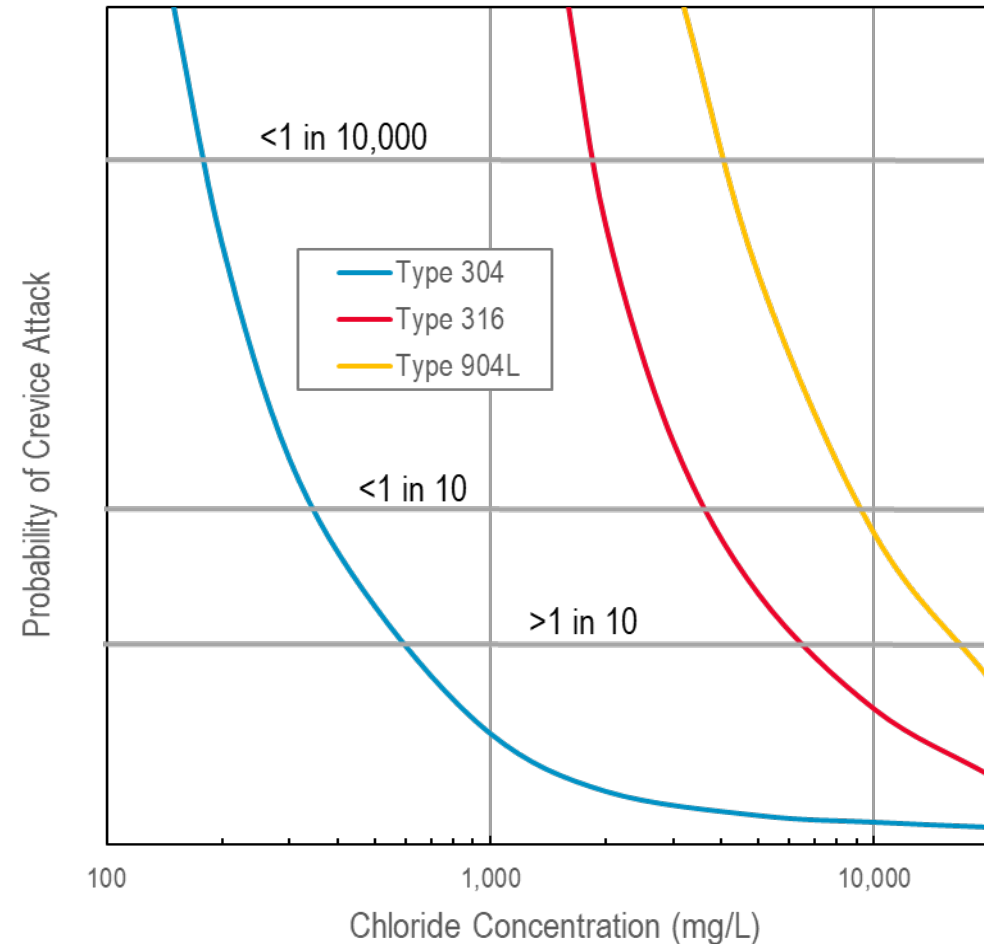


MAR Well Design Parameters and Features

- Recharge rate – 2 mgd
- Backflush rate – 3 mgd
- Accommodate 15-in diameter vertical turbine pump w/ 10-in diameter column pipe
- Backflush pump column length – 300 linear feet
- Outer casing depth – approx. 400 feet bgs
- In-line orifice to control recharge
- Separate external 2" SST monitoring pipe to accommodate instrumentation

Corrosive NGW and Extended Startup

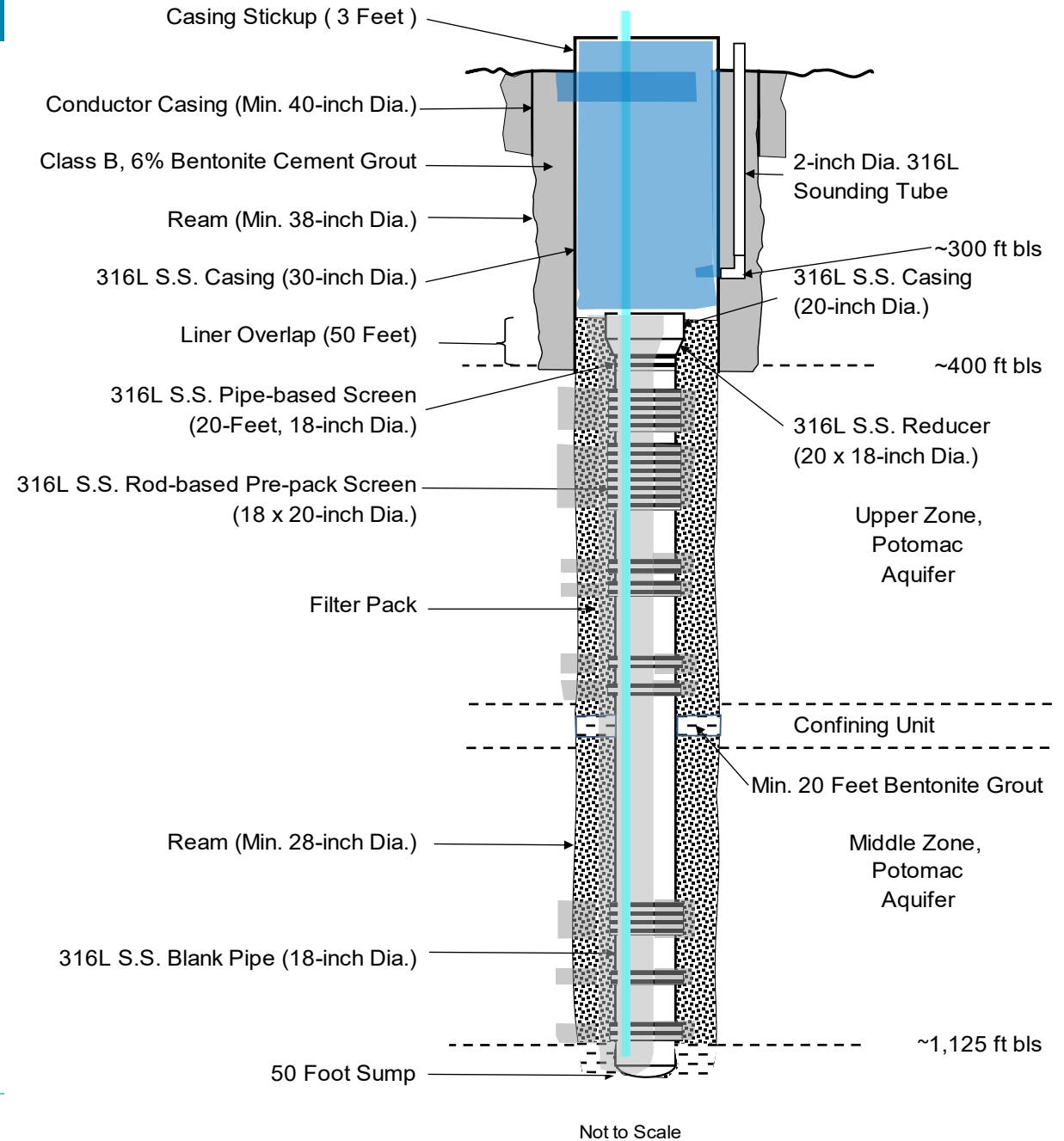
- Middle Potomac Aquifer chloride concentration up to 4,500 mg/L
- Potential for uphole migration into UPA
- Shut-in period could exceed 4 years for the on-site wells
- Type 316 SS suitable to 3,000 mg/L chloride



Source: Nickel Development Institute, 1987. Nickel stainless steels for marine environments, natural waters and brines.

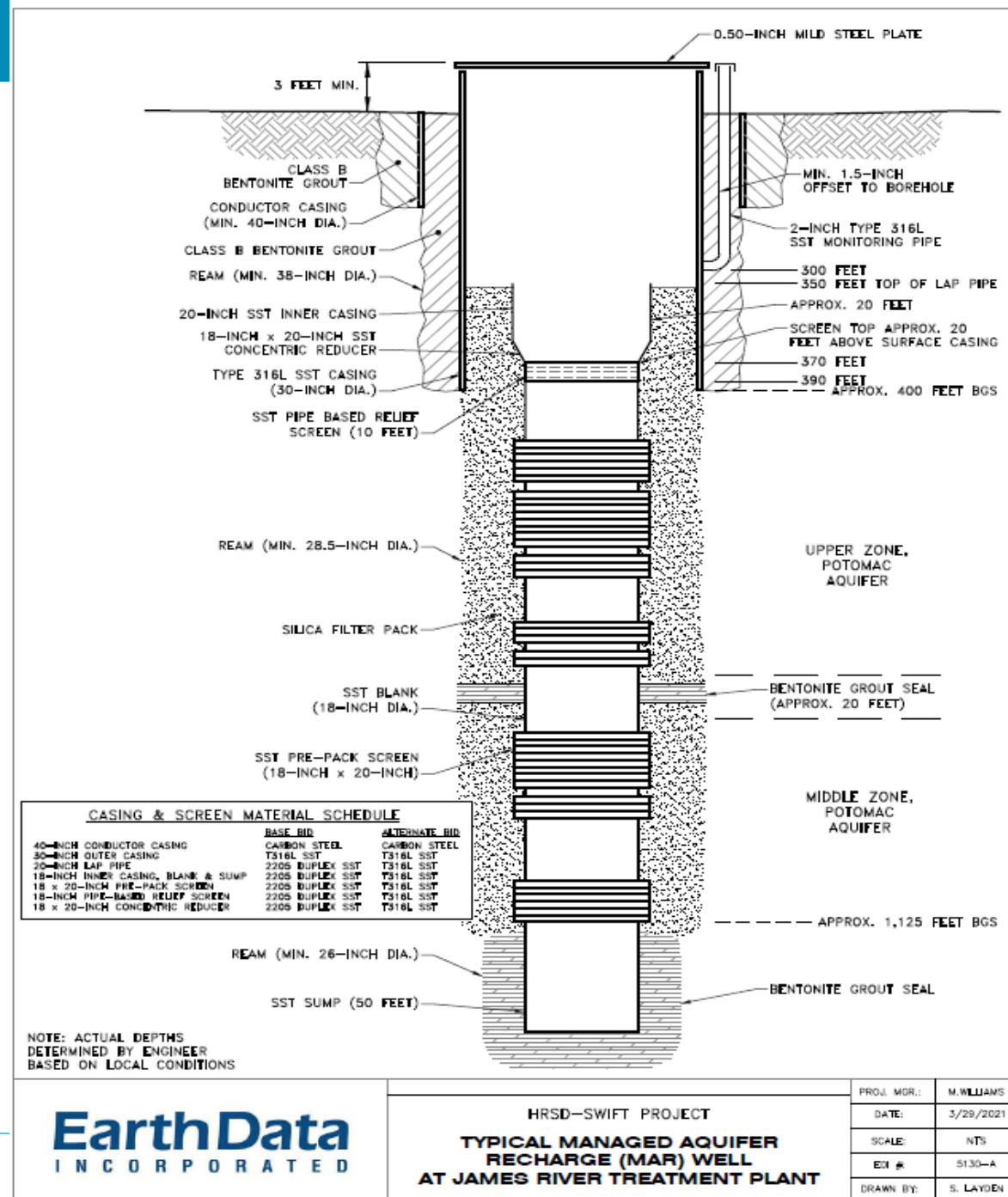
Solutions

- Use 2205 Duplex SS for recharge string (JRTP on-site wells only)
 - Cost \approx 4 x 316L SS)
- Change the well environment
 - freshwater-based sodium bentonite suspension
 - placed from base of sump to top recharge string
 - freshwater placed from surface in upper casing and external monitoring pipe



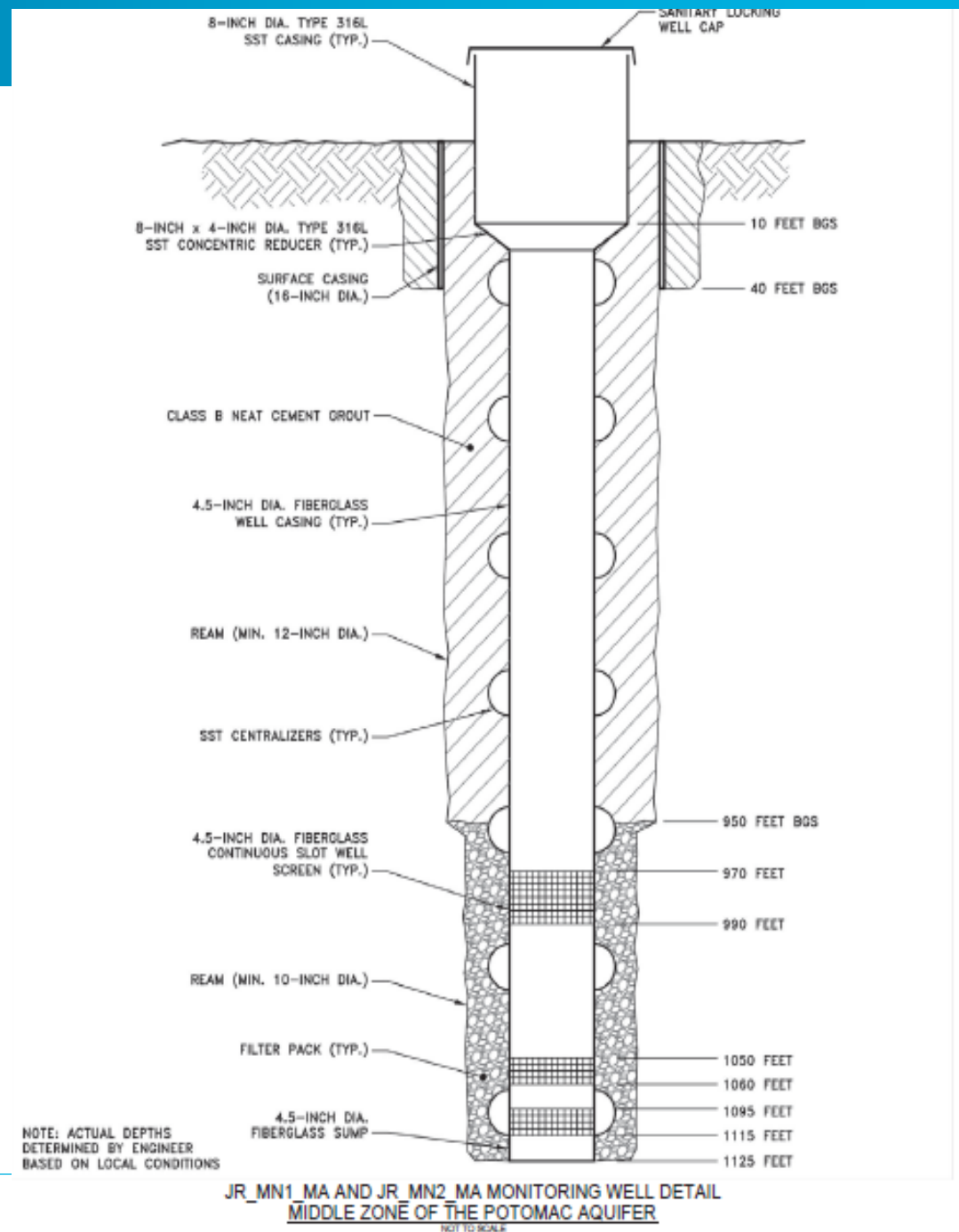
JRTP MAR Well Design Details

- 2-piece construction allows for future filter pack augmentation
- 40" steel surface casing
- 30" SST outer casing
- 20" liner swedge to 18" to facilitate liner rehab
- 18" pipe-based relief screen
- 18" X 20" SST pre-pack recharge screen & 18" SST inner casing & sump based on pilot hole and geophysical logs
- 50' sump for extended run times between potential well rehab events
- 20' thick bentonite seal between UPA and MPA for zone isolation



MW Design Parameters and Features

- Four MWs in close proximity to each other at four different depths
 - Approx. 500', 700', 800' and 1,200'
 - Three MWs completed in the Upper Zone of the Potomac Aquifer and one in Middle Zone
- 8" SST upper casing & 4.5" FRP casing and continuous slot screen
- Baseline pumping test data & water quality sampling
- Permanent sampling pumps to be installed to facilitate regular compliance sampling by HRSD
- Level monitoring – single pressure transducer



HRSD SWIFT - JAMES RIVER WWTP

JRMN2 CLUSTER MONITORING WELLS
 PRELIMINARY ESTIMATED SCREEN PICKS
 4/25/2023 - DRAFT UA & UB and Finalized JR_MN2_MA & UC

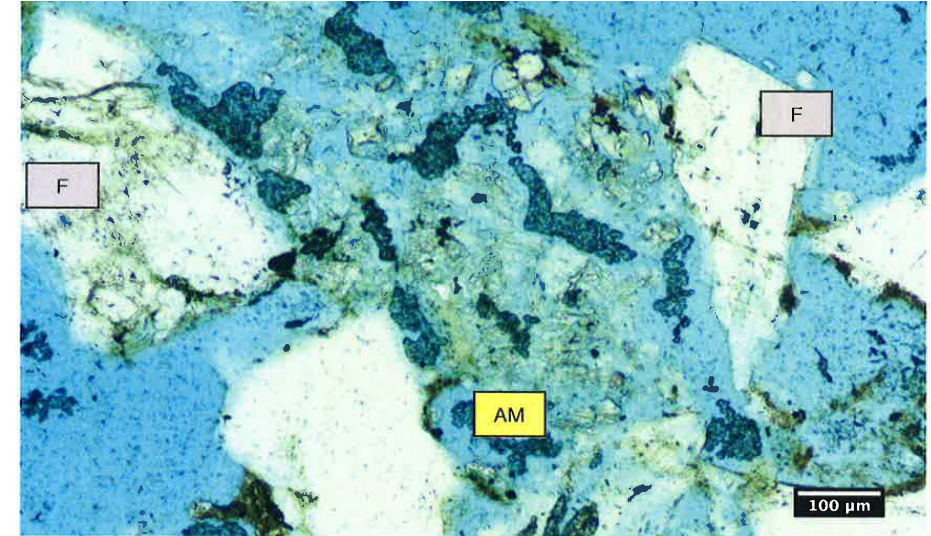
| Based on JRMN2_MA Geophysical Log and Nearest JR_MAR Wells | | | | | | | |
|--|----------------------------|----------|-----------|--------------|----|----------|-----------------------|
| MN_ZONE | WELL ID | Screen # | Top Depth | Bottom Depth | LF | Total LF | Status |
| UzA of PA | JR_MN2_UA DEQ:216-00136 | 1 | 425 | 440 | 15 | 20 | DRAFT |
| | | 2 | 488 | 493 | 5 | | |
| UzB of PA | JR_MN2_UB DEQ:216-00137 | 1 | 513 | 528 | 15 | 45 | DRAFT |
| | | 2 | 548 | 553 | 5 | | |
| | | 3 | 590 | 600 | 10 | | |
| | | 4 | 630 | 635 | 5 | | |
| | | 5 | 682 | 692 | 10 | | |
| UzC of PA | JR_MN2_UC DEQ:216-00138 | 1 | 744 | 754 | 10 | 20 | FINAL |
| | | 2 | 795 | 805 | 10 | | |
| MzA of PA | JR_MN2_MA DEQ:216-00135 | 1 | 938 | 953 | 15 | 60 | FINAL DEQ Approved |
| | | 2 | 990 | 1010 | 20 | | |
| | | 3 | 1115 | 1130 | 15 | | |
| | | 4 | 1142 | 1147 | 5 | | |
| | | 5 | 1233 | 1238 | 5 | | |

TOTAL SCREEN LENGTH (FT.) 145

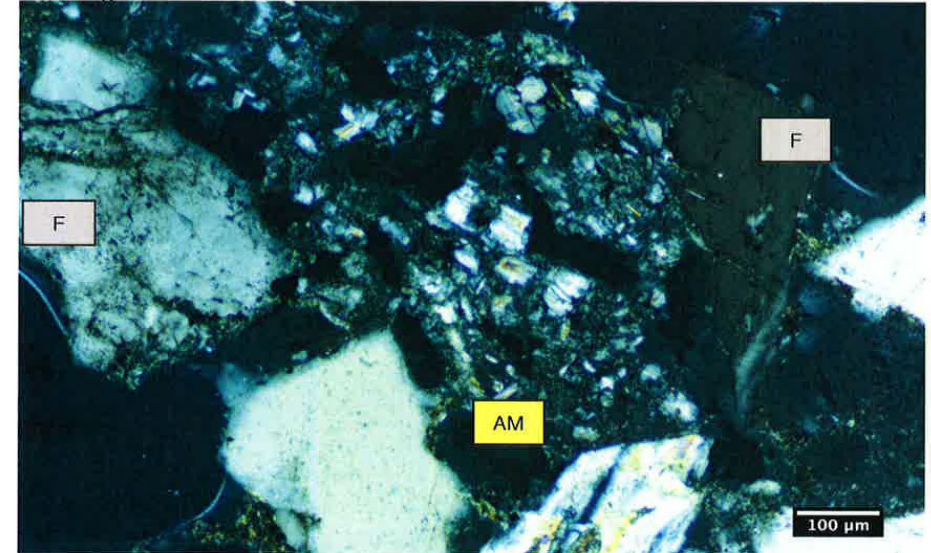
- UzA PA = Upper zone of Potomac aquifer - subzone A: JR_MN2_UA
- UzB PA = Upper zone of Potomac aquifer - subzone B: JR_MN2_UB
- UzC PA = Upper zone of Potomac aquifer - subzone C: JR_MN2_UC
- MzA PA = Middle zone of Potomac aquifer - undifferentiated: JR_MN2_MA

Clay Stability

- Iron oxides, clay minerals, and quartz overgrowths in pores
- Montmorillonite primary clay mineral w/ minor kaolinite and illite/mica in recharge zones
- JR SWIFT ionic strength (IS) = $1.1e-02$
- UPA IS = $7.5e-02$
- MPA IS = $1.1e-01$
- Potential for clay fragmentation



5E. Corroded feldspar (F) partially replaced with authigenic clay matrix (AM) - including kaolinite + montmorillonite.



Recharge Zone Conditioning

- Procedure developed during previous pilot testing at SWIFT sites
- NSF 60 Aluminum chlorohydrate (ACH) solution batched onsite (0.05 molar solution)
- Applied using straddle packers (up to 3 screen intervals) going from bottom to top screen
- 14-day minimum contact period
- Evacuate treated zones through packers
- Post-conditioning pumping tests compared to baseline well hydraulics





**HRSD SWIFT - JAMES RIVER WWTP
PROPOSED ACH TREATMENT AT 0.05 Molar Concentration
WELL JR_MAR_04 (DEQ 216-00124)**

Summary of Treatment Zones at James River
Treatment Volumes ACH 14 feet into aquifer

Volume of 18-inch casing
Volume of 6-inch T&C pipe

12.14 gal/ft (17.25 I.D.)
1.50 gal/ft (6.065 I.D.)

| Aquifer | Packed Zone | Screen Top | Screen Bottom | Screen Interval Length | Total Length of screen | Packer Zone Top | Packer Zone Bottom | Total Length of Zone | Treatment Radius | Volume treatment | Volume of water to evacuate | Volume ACH | |
|----------------------------|-------------|------------|---------------|------------------------|------------------------|-----------------|--------------------|----------------------|------------------|------------------|-----------------------------|------------|---------|
| | Number | (fbg) | (fbg) | (ft) | (ft) | (fbg) | (fbg) | (feet) | (ft) | fluid (gallons) | (gallons) | (gallons) | (totes) |
| Upper Zone of the Potomac | 1 | 408 | 440 | 32 | | 398 | - | 61 | 14 | 36,748 | 1,413 | 524 | 2.2 |
| | 2 | 448 | 458 | 10 | 42 | - | 459 | 61 | 14 | 92,744 | 2,315 | 1323 | 5.5 |
| | | 556 | 592 | 36 | 106 | - | 596 | 122 | | | | | |
| | 3 | 620 | 650 | 30 | 30 | 615 | 676 | 61 | 14 | 26,248 | 1,671 | 374 | 1.6 |
| 4 | 734 | 754 | 20 | | 698 | - | | 122 | 14 | 41,997 | 2,639 | 599 | 2.5 |
| | 772 | 800 | 28 | 48 | - | 820 | | | | | | | |
| Middle Zone of the Potomac | 5 | 962 | 1022 | 60 | 60 | 925 | 1047 | 122 | 14 | 52,497 | 2,924 | 749 | 3.1 |
| | 6 | 1064 | 1074 | 10 | | 1054 | - | | 14 | 40,247 | 3,212 | 574 | 2.4 |
| | | 1112 | 1138 | 26 | | - | - | | | | | | |
| | | 1154 | 1164 | 10 | 46 | - | 1176 | 122 | | | | | |

Aluminum Chlorohydrate (ACH)

0.05 M

29 gallons per 1,000 gallons H₂O

290,481

14,173

4,142

17

Porosity (fraction) 0.19

Draft Calculation: 8/29/2023

- 290481 Total Treatment fluid (gallons)
- 4203 MINUS ACH volume (gallons)
- 286277 Treatment fluid minus ACH (gallons)
- 4142 ACH volume needed (gallons)
- 17 Totes
- 240 gallon/tote
- 14.5 gallons of ACH per 1,000 gallon solution

Comparison of Pre-and Post-ACH Specific Capacity and Turbidity in JR_MAR_01 and JR_MAR_03 (Preliminary Data)

| | JR_MAR_01 | JR_MAR_03 |
|---|-----------|-----------|
| Pre-ACH pumping test rate (gpm) | 1795 | 1500 |
| Pre-ACH 60-minute specific capacity (gpm/ft) | 78.10 | 66.80 |
| Pre-ACH turbidity (NTU) | 1.91 | 3.41 |
| Post-ACH pumping test rate (gpm) | 1795 | 1500 |
| Post-ACH 60-minute specific capacity (gpm/ft) | 73.90 | 44.60 |
| Post-ACH turbidity (NTU) | 1.84 | 1.96 |
| Specific capacity change | -4.2 | -22.2 |
| Specific capacity % change | -5.4% | -33.2% |

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